

Q1: Starting with general TL equations in time-domain, 1
 derive the TL wave equation for current $i(z, t)$

Sol: TL general equations are given by

$$\textcircled{1} \frac{\partial v(z, t)}{\partial z} = -R i(z, t) - L \frac{\partial i(z, t)}{\partial t} \quad \&$$

$$\textcircled{2} \frac{\partial i(z, t)}{\partial z} = -C \frac{\partial v(z, t)}{\partial t} - G v(z, t) \quad \text{let } i(z, t) \equiv i$$

$$\textcircled{3} v(z, t) \equiv v$$

$$\& \text{ take } \frac{\partial}{\partial z} \text{ of (2)} \Rightarrow \textcircled{4} \frac{\partial^2 i}{\partial z^2} = -C \frac{\partial}{\partial t} \frac{\partial v}{\partial z} - G \frac{\partial v}{\partial z} \quad \text{where } \textcircled{5} \frac{\partial}{\partial z} \frac{\partial}{\partial t} = \frac{\partial}{\partial t} \frac{\partial}{\partial z}$$

Sub (1) in (4) \Rightarrow

$$\textcircled{6} \frac{\partial^2 i}{\partial z^2} = -C \frac{\partial}{\partial t} \left[-R i - L \frac{\partial i}{\partial t} \right] - G \left[-R i - L \frac{\partial i}{\partial t} \right]$$

$$\textcircled{7} \frac{\partial^2 i}{\partial z^2} = CR \frac{\partial i}{\partial t} + CL \frac{\partial^2 i}{\partial t^2} + GR i + GL \frac{\partial i}{\partial t} \Rightarrow$$

$$\boxed{\frac{\partial^2 i(z, t)}{\partial z^2} = LC \frac{\partial^2 i(z, t)}{\partial t^2} + (GL + RC) \frac{\partial i(z, t)}{\partial t} + GR i(z, t)}$$

which is given in your notes.

Q2: Derive the TL wave equation for current in sinusoidal steady state form.

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Sol: From previous question we have

$$\textcircled{1} \quad \frac{\partial^2 i(z,t)}{\partial z^2} = LC \frac{\partial^2 i(z,t)}{\partial t^2} + (GL + RC) \frac{\partial i(z,t)}{\partial t} + GR i(z,t)$$

Let's use harmonic fields: $i(z,t) = \text{Re}[\bar{I}(z) e^{j\omega t}] = \text{Re}[I e^{j\phi(z)} e^{j\omega t}]$

then (1) \Rightarrow $\textcircled{3}$

$$\frac{\partial^2}{\partial z^2} \text{Re}[\bar{I}(z) e^{j\omega t}] = LC \frac{\partial^2}{\partial t^2} \text{Re}[\bar{I}(z) e^{j\omega t}] + (GL + RC) \frac{\partial}{\partial t} \text{Re}[\bar{I}(z) e^{j\omega t}] + GR \text{Re}[\bar{I}(z) e^{j\omega t}] \Rightarrow$$

$\textcircled{4}$

$$\text{Re}[e^{j\omega t} \frac{\partial^2 \bar{I}(z)}{\partial z^2}] = LC \text{Re}[\bar{I}(z) \frac{\partial^2 e^{j\omega t}}{\partial t^2}] + (GL + RC) \text{Re}[\bar{I}(z) \frac{\partial e^{j\omega t}}{\partial t}] + GR \text{Re}[\bar{I}(z) e^{j\omega t}] \Rightarrow$$

$\textcircled{5}$

$$\text{Re}[e^{j\omega t} \frac{\partial^2 \bar{I}(z)}{\partial z^2}] = LC \text{Re}[-\omega^2 \bar{I}(z) e^{j\omega t}] + (GL + RC) \text{Re}[\bar{I}(z) j\omega e^{j\omega t}] + GR \text{Re}[\bar{I}(z) e^{j\omega t}] \Rightarrow$$

$\textcircled{6}$

$$\text{Re}[e^{j\omega t} \frac{\partial^2 \bar{I}(z)}{\partial z^2}] = \text{Re}[-\omega^2 LC \bar{I}(z) e^{j\omega t} + (GL + RC) \bar{I}(z) j\omega e^{j\omega t} + GR \bar{I}(z) e^{j\omega t}] \Rightarrow$$

From properties of phasor we have

$$\textcircled{1} \quad \cancel{e^{j\omega t}} \frac{d^2}{dz^2} \bar{I}(z) = -\omega^2 L C \bar{I}(z) \cancel{e^{j\omega t}} + (GL + RC) \bar{I}(z) \cancel{e^{j\omega t}} + \underline{\underline{3}} \\ RG \bar{I}(z) \cancel{e^{j\omega t}} \Rightarrow$$

$$\textcircled{2} \quad \frac{d^2}{dz^2} \bar{I}(z) = [-\omega^2 LC + (GL + RC)j\omega + RG] \bar{I}(z)$$

Note that $\textcircled{3} \quad \kappa^2 = (G + j\omega C)(R + j\omega L) = RG - \omega^2 LC + j(\omega CR + \omega LG)$

hence (2) can be written as

$$\frac{d^2}{dz^2} \bar{I}(z) = \kappa^2 \bar{I}(z) \text{ or given in your notes.}$$

Q3: Prove that solution to $\frac{d^2 \bar{V}(z)}{dz^2} = \kappa^2 \bar{V}(z)$ is

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given by $\textcircled{2} \bar{V}(z) = V_0^+ e^{-\kappa z} + V_0^- e^{+\kappa z}$

Sol: To prove that $\textcircled{2}$ is a solution let us calculate the

$\frac{d \bar{V}(z)}{dz}$ & hence $\frac{d^2 \bar{V}(z)}{dz^2}$

$\textcircled{3} \frac{d \bar{V}(z)}{dz} = -\kappa V_0^+ e^{-\kappa z} + \kappa V_0^- e^{+\kappa z}$ &

$\textcircled{4} \frac{d^2 \bar{V}(z)}{dz^2} = \kappa^2 V_0^+ e^{-\kappa z} + \kappa^2 V_0^- e^{+\kappa z} = \kappa^2 [V_0^+ e^{-\kappa z} + V_0^- e^{+\kappa z}]$

$\textcircled{4} \Rightarrow \frac{d^2 \bar{V}(z)}{dz^2} = \kappa^2 \bar{V}(z)$ which is the desired result

Q4: For a distortionless line, find the propagation constant, attenuation constant, phase constant, phase velocity & characteristic impedance

Sol: For distortionless line $\textcircled{1} \frac{R}{G} = \frac{L}{C} \Rightarrow \textcircled{2} \frac{R}{L} = \frac{G}{C}$

Recall $\textcircled{2} \gamma = \sqrt{(R+j\omega L)(G+j\omega C)} \Rightarrow \textcircled{3} \gamma = \sqrt{L(\frac{R}{L}+j\omega)C(\frac{G}{C}+j\omega)} \Rightarrow$

$\textcircled{4} \gamma = \sqrt{LC(\frac{R}{L}+j\omega)(\frac{R}{L}+j\omega)} = \sqrt{LC}(\frac{R}{L}+j\omega) = R\sqrt{\frac{C}{L}} + j\omega\sqrt{LC}$

then $\textcircled{5} \boxed{\beta = \omega\sqrt{LC}}, \boxed{\alpha = R\sqrt{\frac{C}{L}}} \textcircled{7} \boxed{V_p = \frac{\omega}{\beta} = \frac{1}{\sqrt{LC}}}$

also $Z_0 = \sqrt{\frac{R+j\omega L}{G+j\omega C}}$ For distortionless line $Z_0 = \sqrt{\frac{L(\frac{R}{L}+j\omega)}{C(\frac{G}{C}+j\omega)}} = \sqrt{\frac{L}{C}}$

$\Rightarrow Z_0 = R_0 = jX_0 = \sqrt{\frac{L}{C}} \Rightarrow R_0 = \sqrt{\frac{L}{C}}, X_0 = 0$

* Note that aside a non-vanishing attenuation constant (α) the other parameters of a distortionless line is the same as the lossless line (i.e β, V_p, R_0 , & X_0 are the same.)

Q5: Figure shows two charged conductors immersed in a lossy dielectric of conductivity σ & dielectric constant ϵ . 6

a) show that the following expression holds

$$\textcircled{1} RC = \frac{C}{G} = \frac{\epsilon}{\sigma} \quad \text{where } \textcircled{2} R = \frac{1}{G} \text{ is the resistance}$$

associated with the lossy dielectric, & C the capacitance between the two conductors

b) From the result in part (a) find the leakage resistance (conductance per unit length) of a coaxial cable of inner radius a & outer radius b .

Sol:

(a). The definition for capacitance between two conductors is given by

$$\textcircled{1} C = \frac{Q}{V} = \frac{\oint_S \vec{D} \cdot d\vec{s}}{-\int_L \vec{E} \cdot d\vec{l}}$$



lossy dielectric (ϵ, σ)

where \oint_S (surface integral) is carried over the surface enclosing the +tively charged conductor & \int_L (line integral) is carried from -tively charged conductor (lower potential) to the +tively charged conductor (higher potential)

* When the dielectric between conductors is lossy (not a perfect insulator) a current will flow from one conductor to the other. If medium is isotropic this current & electric field between the two conductors are co-linear since $\vec{J} = \sigma \vec{E}$, where σ is the conductivity associated with our lossy (not perfect) dielectric. In other words, there will be a resistance between the two conductors, which is called the leakage resistance, its value is given by

$$(4) \quad R = \frac{V}{I} = \frac{-\int_L \vec{E} \cdot d\vec{l}}{\iint_{S'} \vec{J} \cdot d\vec{s}}$$

where \int_L (line integral) & \iint_S (surface integral) are carried over the same path & surface or before.

* multiply (4) & (3-P6) we have

$$(5) \quad RC = \frac{\iint_S \vec{D} \cdot d\vec{s}}{-\int_L \vec{E} \cdot d\vec{l}} \cdot \frac{-\int_L \vec{E} \cdot d\vec{l}}{\iint_{S'} \vec{J} \cdot d\vec{s}} = \frac{\iint_S \epsilon \vec{E} \cdot d\vec{s}}{\iint_{S'} \sigma \vec{E} \cdot d\vec{s}} \quad \text{where } \begin{matrix} (6) \vec{D} = \epsilon \vec{E} & (7) \vec{J} = \sigma \vec{E} \end{matrix}$$

If ϵ & σ are position independent, i.e. medium is homogeneous - then.

$$(6) \quad \boxed{RC = \frac{\epsilon}{\sigma}} \Rightarrow \boxed{\frac{C}{G} = \frac{\epsilon}{\sigma}} \quad (7)$$

b) For coaxial cable, we know from electrostatic $C' = \frac{2\pi\epsilon L}{\ln(b/a)}$ (1)



Where ϵ is the permittivity of medium between the two conductors.

Then capacitance per unit length $C' = \frac{C'}{L}$ [F/m] is (2)

(3) $C' = \frac{2\pi\epsilon}{\ln(b/a)}$ [F/m]. From results in part (a) we have

$$(4) \quad \frac{C}{G} = \frac{\epsilon}{\sigma} \Rightarrow \frac{1}{G} \frac{2\pi\epsilon}{\ln(b/a)} = \frac{\epsilon}{\sigma} \Rightarrow$$

$$G = \frac{2\pi\sigma}{\ln(b/a)} \left[\frac{1}{\Omega \cdot m} = \frac{S}{m} \right]$$



$$\oint \vec{D} \cdot d\vec{s} = Q$$

$$\oint \vec{E} \cdot d\vec{s} = Q/\epsilon$$

$$E = E_p \hat{a}_p$$

$$d\vec{l} = dp \hat{a}_p + p d\phi \hat{a}_\phi + dz \hat{a}_z$$

$$ds \text{ here} = p d\phi dz \hat{a}_p \text{ then}$$

$$\oint \vec{E} \cdot d\vec{s} = \int_{\phi=0}^{2\pi} \int_{z=0}^L E_p \hat{a}_p \cdot p d\phi dz$$

$$= E_p p 2\pi L \Rightarrow$$

$$E_p (p 2\pi L) = \frac{Q}{\epsilon} \Rightarrow$$

$$\boxed{\vec{E} = \frac{Q}{2\pi\epsilon L p} \hat{a}_p}$$

$$C' = Q/V$$

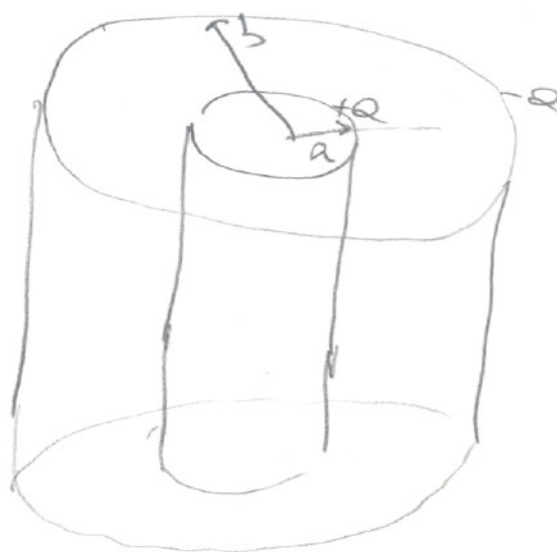
calculate V from lower to higher potential

$$E = - \int_{p=b}^{p=a} \vec{E} \cdot d\vec{l} = - \int_{p=b}^{p=a} \frac{Q \hat{a}_p}{2\pi\epsilon L p} \cdot dp \hat{a}_p$$

$$= \frac{-Q}{2\pi\epsilon L} \left[\ln p \right]_b^a = \frac{-Q}{2\pi\epsilon L} [\ln(a) - \ln(b)]$$

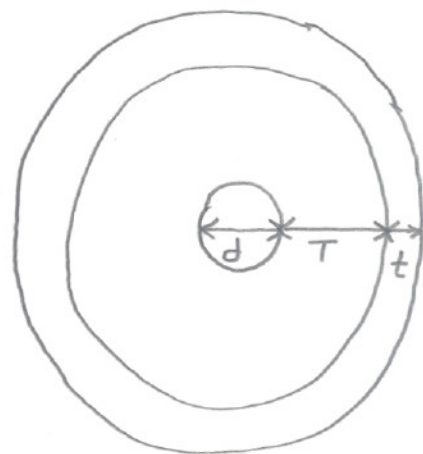
$$= \frac{Q}{2\pi\epsilon L} [\ln(b) - \ln(a)] = \frac{Q}{2\pi\epsilon L} \ln\left(\frac{b}{a}\right)$$

$$C' = \frac{Q}{V} = \frac{Q \cdot 2\pi\epsilon L}{Q \ln(b/a)} = \frac{2\pi\epsilon L}{\ln(b/a)}$$



Q6: Figure shows a RG 58C/U Coaxial Cable, idealized to solid outer conductor. Let us assume that cable is a low loss (high frequency limit) TL with characteristic impedance of $Z_0 = 50 \Omega$.

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Inner conductor: Copper
 $d = 0.9 \text{ mm}$
 resistivity $= \rho_c = 1.7 \times 10^{-8} \text{ } [\Omega \cdot \text{m}]$

Dielectric: Polyethylene
 $T = 1.02 \text{ mm}$
 resistivity $= \rho_d = 10^{14} \text{ } [\Omega \cdot \text{m}]$
 $\epsilon_r = 2.3$

outer conductor: Copper
 $t = 1. \text{ mm}$

resistivity $= \rho_c = 1.7 \times 10^{-8} \text{ } [\Omega \cdot \text{m}]$

- What is the TL capacitance?
- What is the TL inductance?
- What is the value of the TL resistance?
- What is the TL conductance?
- Find a frequency range for which the high frequency assumption used is valid.

Sol:

a) From question (5) for coaxial cable we

found
$$C' = \frac{2\pi\epsilon}{\ln\left(\frac{T+d/2}{d/2}\right)} = \frac{2\pi \times 8.85 \times 10^{-12} \times 2.3}{\ln\left(\frac{1.02 + 0.9/2}{0.9/2}\right)} \Rightarrow$$

$$C' = 1.08 \times 10^{-10} = 108.04 \text{ [pF/m]}$$

b) For low loss line $Z_0 = R_0 + jX_0 = \sqrt{\frac{L}{C}} + j0$

$$\Rightarrow (Z_0)^2 = (R_0)^2 = \frac{L}{C} \Rightarrow L = Z_0^2 C' = (50)^2 \times 108.04 \times 10^{-12} \Rightarrow$$

$$L = 2.701 \times 10^{-7} = 270.1 \text{ [nH/m]}$$

c) For a metallic rod of length L & area A we have

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$$r = \rho \frac{L}{A} \Rightarrow R = \frac{r}{L} = \frac{\rho}{A} \quad \text{where } \rho \text{ is the resistivity of rod}$$



\therefore For inner conductor

$$R_{in} = \frac{\rho_c}{\pi \left(\frac{d}{2}\right)^2} = \frac{1.7 \times 10^{-8}}{\pi (0.9 \times 10^{-3}/2)^2} = 0.0267 \text{ } [\Omega/\text{m}]$$

\therefore For outer conductor

$$R_{out} = \frac{\rho_c}{\pi \left[\frac{d}{2} + T + t\right]^2 - \pi \left[\frac{d}{2} + T\right]^2} = \frac{1.7 \times 10^{-8}}{\pi \left[\frac{0.9}{2} + 1.02 + 1\right]^2 \times 10^{-6} - \pi \left[\frac{0.9}{2} + 1.02\right]^2 \times 10^{-6}} = 0.0014 \text{ } [\Omega/\text{m}]$$

$$R_{total} = R_{in} + R_{out} = 0.0267 + 0.0014 = 0.0281 \text{ } \Omega/\text{m}$$

Then

$$R_{total} = R_{in} + R_{out} = 0.0267 + 0.0014 = 0.0281 \text{ } \Omega/\text{m}$$

d) From previous question

$$\frac{C}{G} = \frac{\epsilon}{\sigma} \Rightarrow$$

$$G = \frac{d \sigma}{\epsilon} \quad \text{where}$$

$\sigma = \frac{1}{\rho}$ this is the resistivity of our lossy dielectric

$$G = 108.04 \times 10^{-12} \times \frac{1}{10^{-14} \times 8.85 \times 10^{-12} \times 2.3} \Rightarrow$$

$$G = 5.308 \times 10^{-14} \left[\frac{\text{sie}}{\text{m}} \right]$$

e) In deriving the expressions for α , β , R_0 & X_0 in the case of low loss (high frequency limit) we have assumed 11

① $R \ll \omega L$ & ② $G \ll \omega C$. For the numbers we have calculated

We have (1) $\Rightarrow 0.0281 \ll \omega \times 270.1 \times 10^{-9} \Rightarrow 1.04 \times 10^5 \ll \omega$ ③

(2) $\Rightarrow 5.308 \times 10^{-14} \ll \omega \times 108.04 \times 10^{-12} \Rightarrow 0.0005 \ll \omega$ ④

we note that at RF & microwave frequencies, the condition $\omega \gg 0.005$ Hz is easily satisfied. As for the condition $\omega \gg 1.04 \times 10^5$ we take \Rightarrow to mean at least 10 times & hence $\omega \gg 1.04 \times 10^6 \Rightarrow \omega \gg 1.655 \times 10^5 = 0.1655$ MHz should be o.k.

Q 7: The attenuation constant of a $50[\Omega]$ distortionless line is $0.01[\text{dB/m}]$ & its capacitance is $0.1[\text{nF/m}]$. 12

a) What are the values of the line resistance, conductance & inductance per meter

b) What is the value of the phase velocity of the propagating waves.

c) What are the ratios of the magnitude of the propagating fields at 1 km & 5 km with respect to the starting point at $z=0$

Sol: For a distortionless line $\textcircled{1} \frac{R}{L} = \frac{G}{C}$ & $\textcircled{2} Z_0 = R_0 + jX_0$ & $\textcircled{3} \gamma = \alpha + j\beta = \sqrt{\frac{C}{L}} (R + j\omega L) = \sqrt{\frac{L}{C}} + 0j$

a) From (2) $L = (Z_0)^2 G' = (50)^2 \times 0.1 \times 10^{-9} = 2.5 \times 10^{-7} [\text{H/m}]$

from (3) $\alpha = \sqrt{\frac{C}{L}} R \Rightarrow R = \alpha \sqrt{\frac{L}{C}} = \frac{0.01}{8.686} \times \sqrt{\frac{2.5 \times 10^{-7}}{0.1 \times 10^{-9}}} \Rightarrow$
 $R = 0.0576 [\Omega/\text{m}]$

from (1) $\Rightarrow G = \frac{C'R}{L} = \frac{0.1 \times 10^{-9} \times 0.0576}{2.5 \times 10^{-7}} = 2303 \times 10^{-5} [\frac{\text{S}}{\text{m}}]$
 $\approx 23.02 [\frac{\mu\text{S}}{\text{m}}]$

$$b) \quad V_p = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{2.5 \times 10^{-7} \times 0.1 \times 10^{-9}}} = 2 \times 10^8 \text{ m/s} = 0.667c$$

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Where c is the speed of light in vacuum.

$$c) \quad \frac{V(z=1000)}{V(z=0)} = \frac{|V_0^+ e^{-\alpha z} e^{-j\beta z}|}{|V_0^+ e^0 e^0|} = e^{-\alpha z}$$

$$\alpha = \frac{0.01}{8.686} = 1.151 \times 10^{-3} \text{ [NP/m]}$$

$$\text{then } \frac{V(z=1000\text{m})}{V(z=0)} = e^{-1.151 \times 10^{-3} \times 10^3} = e^{-1.151} = 0.316 = 32\%$$

$$\frac{V(z=5000\text{m})}{V(z=0)} = e^{-1.151 \times 10^{-3} \times 5 \times 10^3} = e^{-5.756} = 3.162 \times 10^{-3} = 0.32\%$$

Q 8: Use the relation $\alpha = \frac{P_{dis}}{2P(z)}$ to find the Attenuation constant for a low loss line (high frequency limit). 14

Sol: In notes we showed that average power is given by

$$\textcircled{2} P(z) = \frac{1}{2} \frac{|V_0|^2}{|Z_0|^2} R_0 e^{-2\alpha z}$$

* we also note that time-averaged dissipated power is given by

$$\begin{aligned} \textcircled{3} P_{diss} &= \frac{1}{2} \operatorname{Re} [|I(z)|^2 R + |V(z)|^2 G] \\ &= \frac{1}{2} [|I(z)|^2 R + |V(z)|^2 G] \quad \text{since } R \& G \text{ are real.} \end{aligned}$$

* with $\textcircled{4} V(z) = V_0 e^{-\alpha z} e^{-j\beta z} \Rightarrow \textcircled{6} |V(z)|^2 = |V_0|^2 e^{-2\alpha z}$

$\textcircled{5} I(z) = \frac{V_0}{Z_0} e^{-\alpha z} e^{-j\beta z} \Rightarrow \textcircled{7} |I(z)|^2 = \frac{|V_0|^2}{|Z_0|^2} e^{-2\alpha z}$

Then $\textcircled{6} P_{diss} = \frac{1}{2} \left[\frac{|V_0|^2}{|Z_0|^2} e^{-2\alpha z} R + |V_0|^2 e^{-2\alpha z} G \right]$
 $= \frac{1}{2} \frac{|V_0|^2}{|Z_0|^2} e^{-2\alpha z} [R + |Z_0|^2 G]$

Use (6) & (2) in (1) \Rightarrow

$$\alpha = \frac{\frac{1}{2} \frac{|V_0|^2}{|Z_0|^2} e^{-2\alpha z} [R + |Z_0|^2 G]}{2 \times \frac{1}{2} \frac{|V_0|^2}{|Z_0|^2} e^{-2\alpha z} R_0} = \frac{1}{2} \frac{[R + |Z_0|^2 G]}{R_0}$$

For low loss line $Z_0 = R_0 + jX_0 = \sqrt{\frac{L}{C}} + j0 \Rightarrow$

$Z_0 = R_0 = \sqrt{\frac{L}{C}}$ then

$$\alpha = \frac{1}{2} \frac{[R + \frac{L}{C} G]}{\sqrt{L/C}} = \frac{1}{2} \frac{\sqrt{C}}{\sqrt{L}} [R + G \frac{L}{C}] \Rightarrow$$

$\alpha = \frac{1}{2} [R \sqrt{\frac{C}{L}} + G \sqrt{\frac{L}{C}}]$

 or before