

1(a):

1

* For time harmonic fields $\vec{E} = \text{Re} [\vec{E} e^{j\omega t}] \Rightarrow$

$$\hat{y} E_0 \sin\left(\frac{\pi}{a} x\right) \cos(\omega t - \beta_z z) = \text{Re} \left[E_0 \sin\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} e^{j\omega t} \right] \hat{y}$$

$$\Rightarrow \boxed{\vec{E} = E_0 \sin\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} \hat{y} = E_y \hat{y}}$$

$$\nabla \times \vec{E} = -j\omega \vec{B} \Rightarrow \vec{B} = \frac{j}{\omega} \nabla \times \vec{E} = \frac{j}{\omega} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & E_y & 0 \end{vmatrix}$$

$$= \frac{j}{\omega} \left[-\hat{x} \frac{\partial}{\partial z} E_y + \hat{z} \frac{\partial}{\partial x} E_y \right]$$

$$= \frac{j}{\omega} \left[-\hat{x} E_0 \sin\left(\frac{\pi}{a} x\right) (-j\beta_z) e^{-j\beta_z z} + \right.$$

$$\left. \hat{z} E_0 \frac{\pi}{a} \cos\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} \right]$$

$$= -\frac{\beta_z}{\omega} E_0 \sin\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} \hat{x} + \frac{j}{\omega} E_0 \frac{\pi}{a} \cos\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} \hat{z}$$

Since $\vec{H} = \frac{\vec{B}}{\mu_0}$ then

$$\vec{H} = \frac{-\beta_z}{\omega \mu_0} E_0 \sin\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} \hat{x} + \frac{j E_0}{\omega \mu_0} \left(\frac{\pi}{a}\right) \cos\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} \hat{z} \Rightarrow$$

$$\vec{H} = H_x \hat{x} + H_z \hat{z}$$

$$\text{Hence } \boxed{\vec{H} = \text{Re} [\vec{H} e^{j\omega t}] = -\frac{\beta_z}{\omega \mu_0} E_0 \sin\left(\frac{\pi}{a} x\right) \cos(\omega t - \beta_z z) \hat{x} + \frac{E_0}{\omega \mu_0} \left(\frac{\pi}{a}\right) \cos\left(\frac{\pi}{a} x\right) \sin(\omega t - \beta_z z + \frac{\pi}{2}) \hat{z}}$$

OR

$$\vec{H} = -\frac{\beta_z}{\omega \mu_0} E_0 \sin\left(\frac{\pi}{a} x\right) \cos(\omega t - \beta_z z) \hat{x}$$

$$- \frac{E_0}{\omega \mu_0} \left(\frac{\pi}{a}\right) \cos\left(\frac{\pi}{a} x\right) \sin(\omega t - \beta_z z) \hat{z}$$

1: (b)

From Ampere's law we have

$$\nabla \times \vec{H} = \vec{J} + j\omega \epsilon_0 \vec{E} \rightarrow \nabla \times \vec{H} = j\omega \epsilon_0 \vec{E} \quad \text{here}$$

2

$$\vec{H} = H_x \hat{x} + H_z \hat{z} \quad \text{then} \quad \nabla \times \vec{H} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ H_x & 0 & H_z \end{vmatrix} \Rightarrow$$

$$\nabla \times \vec{H} = \hat{x} \frac{\partial}{\partial y} H_z - \hat{y} \left(\frac{\partial}{\partial x} H_z - \frac{\partial}{\partial z} H_x \right)$$

$$- \hat{z} \left(\frac{\partial}{\partial y} H_x \right) = \hat{y} \left(\frac{\partial}{\partial z} H_x - \frac{\partial}{\partial x} H_z \right) \quad \& \text{ since}$$

$$\nabla \times \vec{H} = j\omega \epsilon_0 \vec{E} \Rightarrow \hat{y} \left(\frac{\partial}{\partial z} H_x - \frac{\partial}{\partial x} H_z \right) = j\omega \epsilon_0 E_y \hat{y} \Rightarrow$$

$$\frac{j\beta_z}{\omega \mu_0} E_0 \sin\left(\frac{\pi}{a} x\right) (-j\beta_z) e^{-j\beta_z z} + \frac{jE_0}{\omega \mu_0} \left(\frac{\pi}{a}\right)^2 \sin\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} =$$

$$j\omega \epsilon_0 E_0 \sin\left(\frac{\pi}{a} x\right) e^{-j\beta_z z} \Rightarrow$$

$$\frac{j\beta_z^2}{\omega \mu_0} + \frac{j}{\omega \mu_0} \left(\frac{\pi}{a}\right)^2 = j\omega \epsilon_0 \Rightarrow$$

$$\beta_z^2 + \left(\frac{\pi}{a}\right)^2 = \omega^2 \mu_0 \epsilon_0 \Rightarrow$$

$$\beta_z = \pm \sqrt{\omega^2 \mu_0 \epsilon_0 - \left(\frac{\pi}{a}\right)^2}$$

Problem 2:

① $\nabla\psi = \frac{\partial\psi}{\partial x} \hat{a}_x + \frac{\partial\psi}{\partial y} \hat{a}_y + \frac{\partial\psi}{\partial z} \hat{a}_z$ & From coordinate

transformation we have

②
$$\begin{bmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} = \begin{bmatrix} A_\rho \\ A_\phi \\ A_z \end{bmatrix}$$

When $\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z = A_\rho \hat{a}_\rho + A_\phi \hat{a}_\phi + A_z \hat{a}_z$ - Using (2)

the vector $\nabla\psi$ given in Cartesian coordinate can be transformed to cylindrical coordinate according to

③
$$\begin{bmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \partial\psi/\partial x \\ \partial\psi/\partial y \\ \partial\psi/\partial z \end{bmatrix} = \begin{bmatrix} \nabla_\rho \\ \nabla_\phi \\ \nabla_z \end{bmatrix} \Rightarrow$$

) $\nabla_\rho = \cos\phi \frac{\partial\psi}{\partial x} + \sin\phi \frac{\partial\psi}{\partial y}$

) $\nabla_\phi = -\sin\phi \frac{\partial\psi}{\partial x} + \cos\phi \frac{\partial\psi}{\partial y}$

) $\nabla_z = \frac{\partial\psi}{\partial z}$

$\Rightarrow$ ⑦ $\nabla\psi(\rho, \phi, z) = \nabla_\rho \psi(\rho, \phi, z) \hat{a}_\rho + \nabla_\phi \psi(\rho, \phi, z) \hat{a}_\phi + \nabla_z \psi(\rho, \phi, z) \hat{a}_z$

By chain rule

⑧ $\frac{\partial\psi}{\partial x} = \frac{\partial\psi}{\partial\rho} \frac{\partial\rho}{\partial x} + \frac{\partial\psi}{\partial\phi} \frac{\partial\phi}{\partial x} + \frac{\partial\psi}{\partial z} \frac{\partial z}{\partial x}$

⑨ $\frac{\partial\psi}{\partial y} = \frac{\partial\psi}{\partial\rho} \frac{\partial\rho}{\partial y} + \frac{\partial\psi}{\partial\phi} \frac{\partial\phi}{\partial y} + \frac{\partial\psi}{\partial z} \frac{\partial z}{\partial y}$

Therefore, we need to calculate $\frac{\partial P}{\partial x}$, $\frac{\partial P}{\partial y}$, $\frac{\partial \phi}{\partial x}$, $\frac{\partial \phi}{\partial y}$ =

* From transformation rule we have

(12) $P = (x^2 + y^2)^{1/2}$ (12) $x = P \cos \phi$

(13) $\phi = \tan^{-1}(y/x)$ (13) $y = P \sin \phi$

(14) then $\frac{\partial P}{\partial x} = \frac{1}{2} (x^2 + y^2)^{-1/2} \times 2x = \frac{x}{(x^2 + y^2)^{1/2}} = \frac{P \cos \phi}{P} = \boxed{\cos \phi}$

(15) $\frac{\partial P}{\partial y} = \frac{1}{2} (x^2 + y^2)^{-1/2} \times 2y = \frac{y}{(x^2 + y^2)^{1/2}} = \frac{P \sin \phi}{P} = \boxed{\sin \phi}$

(16) $\frac{\partial \phi}{\partial x} = \frac{1}{[1 + (y/x)^2]} \times \frac{-y}{x^2} = \frac{-y}{x^2 + y^2} = \frac{-P \sin \phi}{P^2} = \boxed{-\frac{\sin \phi}{P}}$

(17) $\frac{\partial \phi}{\partial y} = \frac{1}{[1 + (y/x)^2]} \times \frac{1}{x} = \frac{x}{(x^2 + y^2)} = \frac{P \cos \phi}{P^2} = \boxed{\frac{\cos \phi}{P}}$

To summarize (18) $\boxed{\frac{\partial P}{\partial x} = \cos \phi}$ (19) $\boxed{\frac{\partial P}{\partial y} = \sin \phi}$ (20) $\boxed{\frac{\partial \phi}{\partial x} = -\frac{\sin \phi}{P}}$

(21) $\boxed{\frac{\partial \phi}{\partial y} = \frac{\cos \phi}{P}}$

* Let us put everything together, i.e. we use (4-5), (8-9), and (18-21)

$$\begin{aligned} \nabla_\rho &= \cos \phi \frac{\partial \psi}{\partial x} + \sin \phi \frac{\partial \psi}{\partial y} = \cos \phi \left[\frac{\partial \psi}{\partial \rho} \frac{\partial \rho}{\partial x} + \frac{\partial \psi}{\partial \phi} \frac{\partial \phi}{\partial x} \right] + \\ &\quad \sin \phi \left[\frac{\partial \psi}{\partial \rho} \frac{\partial \rho}{\partial y} + \frac{\partial \psi}{\partial \phi} \frac{\partial \phi}{\partial y} \right] \\ &= \cos \phi \left[\frac{\partial \psi}{\partial \rho} \cos \phi + \frac{\partial \psi}{\partial \phi} \left(-\frac{\sin \phi}{\rho} \right) \right] + \sin \phi \left[\frac{\partial \psi}{\partial \rho} \sin \phi + \frac{\partial \psi}{\partial \phi} \left(\frac{\cos \phi}{\rho} \right) \right] \\ &= \cos^2 \phi \frac{\partial \psi}{\partial \rho} - \frac{\sin \phi \cos \phi}{\rho} \frac{\partial \psi}{\partial \phi} + \sin^2 \phi \frac{\partial \psi}{\partial \rho} + \frac{\sin \phi \cos \phi}{\rho} \frac{\partial \psi}{\partial \phi} = \frac{\partial \psi}{\partial \rho} \end{aligned}$$

For ∇_ϕ we have

$$\begin{aligned} \nabla_\phi &= -\sin \phi \frac{\partial \psi}{\partial x} + \cos \phi \frac{\partial \psi}{\partial y} = -\sin \phi \left[\frac{\partial \psi}{\partial \rho} \frac{\partial \rho}{\partial x} + \frac{\partial \psi}{\partial \phi} \frac{\partial \phi}{\partial x} \right] + \\ &\quad \cos \phi \left[\frac{\partial \psi}{\partial \rho} \frac{\partial \rho}{\partial y} + \frac{\partial \psi}{\partial \phi} \frac{\partial \phi}{\partial y} \right] \\ &= -\sin \phi \left[\frac{\partial \psi}{\partial \rho} \cos \phi + \frac{\partial \psi}{\partial \phi} \left(-\frac{\sin \phi}{\rho} \right) \right] + \cos \phi \left[\frac{\partial \psi}{\partial \rho} \sin \phi + \frac{\partial \psi}{\partial \phi} \left(\frac{\cos \phi}{\rho} \right) \right] \\ &= -\sin \phi \cos \phi \frac{\partial \psi}{\partial \rho} + \frac{\sin^2 \phi}{\rho} \frac{\partial \psi}{\partial \phi} + \sin \phi \cos \phi \frac{\partial \psi}{\partial \rho} + \frac{\cos^2 \phi}{\rho} \frac{\partial \psi}{\partial \phi} \\ &= \frac{1}{\rho} \frac{\partial \psi}{\partial \phi} \end{aligned}$$

we have seen that $\nabla_z = \frac{\partial}{\partial z} \psi$.

* Then from (7) we have

$$\nabla \psi(\rho, \phi, z) = \frac{\partial \psi(\rho, \phi, z)}{\partial \rho} \hat{\rho} + \frac{1}{\rho} \frac{\partial \psi(\rho, \phi, z)}{\partial \phi} \hat{\phi} + \frac{\partial \psi(\rho, \phi, z)}{\partial z} \hat{z}$$

3)

Ampere law $\Rightarrow$

$$\oint \vec{H} \cdot d\vec{l} = \iint \vec{J}_i \cdot d\vec{s} + \iint \sigma \vec{E} \cdot d\vec{s} + \frac{\partial}{\partial t} \iint \vec{D} \cdot d\vec{s} \Rightarrow$$

①

$$\oint \vec{H} \cdot d\vec{l} = \iint \vec{J}_{ic} \cdot d\vec{s} + \frac{\partial}{\partial t} \iint \vec{D} \cdot d\vec{s}$$

where $\vec{J}_{ic} = \vec{J}_i + \vec{J}_c = \vec{J}_i + \sigma \vec{E}$ ③

The LHS of (2) $\Rightarrow$

$$\lim_{\Delta y \rightarrow 0} \oint \vec{H} \cdot d\vec{l} = \lim_{\Delta y \rightarrow 0} \left\{ \int \vec{H}_1 \cdot d\vec{l} + \int \vec{H}_2 \cdot d\vec{l} \right\} = \lim_{\Delta y \rightarrow 0} \left\{ \vec{H}_1 \Delta x \cdot \hat{a}_x + \vec{H}_2 \Delta x \cdot \hat{a}_x \right\}$$

$$= (\vec{H}_1 - \vec{H}_2) \Delta x \cdot \hat{a}_x$$

The RHS of (2)

As before $\lim_{\Delta y \rightarrow 0} \frac{\partial}{\partial t} \iint \vec{D} \cdot d\vec{s} = \lim_{\Delta y \rightarrow 0} \frac{\partial}{\partial t} \iint \vec{D} \cdot dndy \hat{a}_z = \lim_{\Delta y \rightarrow 0} \left[\frac{\partial}{\partial t} (\vec{D} \cdot \Delta n \Delta y \hat{a}_z) \right]$

$$= 0$$

But

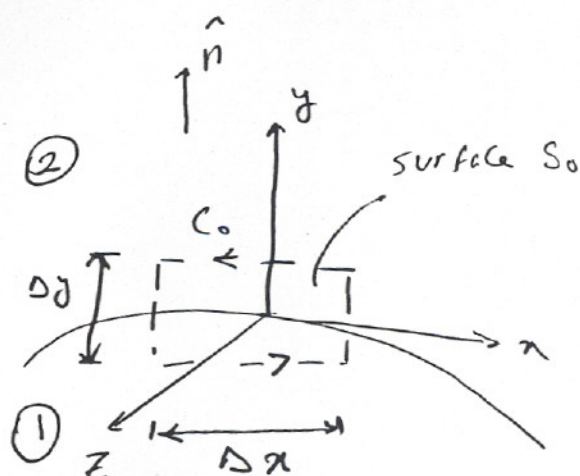
$$\lim_{\Delta y \rightarrow 0} \iint \vec{J}_{ic} \cdot d\vec{s} = \lim_{\Delta y \rightarrow 0} \iint \vec{J}_{ic} \cdot dndy \hat{a}_z = \lim_{\Delta y \rightarrow 0} [\vec{J}_{ic} \Delta x \Delta y] \cdot \hat{a}_z$$

$$= \vec{J}_s \Delta x \cdot \hat{a}_z$$

where

$$\vec{J}_s = \lim_{\Delta y \rightarrow 0} \vec{J}_{ic} \Delta y$$

Putting the RHS & LHS together we have



$$\textcircled{8} (\vec{H}_1 - \vec{H}_2) \cancel{\Delta x} \cdot \hat{a}_x = \vec{J}_s \cancel{\Delta x} \cdot \hat{a}_z$$

Note that $\hat{a}_x = \hat{a}_y \times \hat{a}_z$ then (8) $\Rightarrow$

$$\textcircled{9} (\vec{H}_1 - \vec{H}_2) \cdot (\hat{a}_y \times \hat{a}_z) = \vec{J}_s \cdot \hat{a}_z$$

Recall $\vec{A} \cdot (\vec{B} \times \vec{C}) = \vec{C} \cdot (\vec{A} \times \vec{B})$ (10)

then (9) $\Rightarrow$

$$\textcircled{10} \cancel{\hat{a}_z} \cdot [(\vec{H}_1 - \vec{H}_2) \times \hat{a}_y] = \cancel{\hat{a}_z} \cdot \vec{J}_s \Rightarrow$$

$$\textcircled{11} \hat{a}_y \times (\vec{H}_2 - \vec{H}_1) = \vec{J}_s \quad \text{but from figure it is clear}$$

that $\hat{a}_y = \hat{n} \Rightarrow$

$$\boxed{\hat{n} \times (\vec{H}_2 - \vec{H}_1) = \vec{J}_s}$$

problem 4)

Vector $\vec{M}_1$ is defined by

$$\textcircled{1} \nabla \cdot \vec{M}_1 = S$$

$$\textcircled{2} \nabla \times \vec{M}_1 = \vec{C}$$

$\vec{M}_{in}$

and by its normal component $\sqrt{\text{over a boundary}}$. We want to show that given the above, $\vec{M}_1$ is unique. To do so, let us suppose there is another vector $\vec{M}_2$ that also satisfies all the above conditions. We construct

$$\textcircled{3} \vec{W} = \vec{M}_1 - \vec{M}_2 \text{ \& show that } W=0 \Rightarrow \vec{M}_1 = \vec{M}_2$$

$\textcircled{4}$

Note that $\nabla \cdot \vec{W} = \nabla \cdot (\vec{M}_1 - \vec{M}_2) = \nabla \cdot \vec{M}_1 - \nabla \cdot \vec{M}_2 = S - S = 0$

& $\nabla \times \vec{W} = \nabla \times (\vec{M}_1 - \vec{M}_2) = \nabla \times \vec{M}_1 - \nabla \times \vec{M}_2 = \vec{C} - \vec{C} = 0$

$\textcircled{5}$

Since $\nabla \times \vec{W} = 0 \Rightarrow \textcircled{7} \vec{W} = -\nabla \phi$ use (7) in (4) we have

$$\textcircled{8} \nabla \cdot \vec{W} = \nabla \cdot (-\nabla \phi) = -\nabla \cdot \nabla \phi = -\nabla^2 \phi = 0 \quad \text{Laplace Eq}$$

Green theorem tells us that

$$\textcircled{9} \iint_S U \nabla V \cdot \vec{ds} = \iiint_V U \nabla \cdot \nabla V \, dv + \iiint_V \nabla U \cdot \nabla V \, dv$$

In (9) let $\textcircled{10} U = V = \phi$ then (9) $\Rightarrow$

$$\textcircled{11} \iint_S \phi \nabla \phi \cdot \vec{ds} = \iiint_V \phi \nabla \cdot \nabla \phi \, dv + \iiint_V \nabla \phi \cdot \nabla \phi \, dv$$

Problem 4)

(11) can be written as

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$$(12) \iiint_V \nabla \phi \cdot \nabla \phi \, dV = \iint_S \phi \nabla \phi \cdot \vec{ds} - \iiint_V \phi \nabla \cdot \nabla \phi \, dV$$

However (2) tells us that $\boxed{\nabla \cdot \nabla \phi = \nabla^2 \phi = 0}$ (13)

Also note that $\iint_S \phi \nabla \phi \cdot \vec{ds} = \iint_S \phi (-\vec{W} \cdot \vec{ds}) = - \iint_S \phi (\vec{W} \cdot \vec{ds})$,
↑ from (7)

but what is $\iint_S \phi (\vec{W} \cdot \vec{ds})$? It is the integral of the normal components of $\vec{W}$ ($\vec{W}_n = \vec{M}_{1n} - \vec{M}_{2n}$), and we have supposed that the normal components of $\vec{M}_1$ & $\vec{M}_2$, i.e. $\vec{M}_{1n}$ & $\vec{M}_{2n}$ satisfy the same

boundary conditions $\Rightarrow$

$$(14) \boxed{\begin{aligned} \iint_S \phi \nabla \phi \cdot \vec{ds} &= \iint_S \phi (\vec{W} \cdot \vec{ds}) \\ &= \iint_S \phi (M_{1n} - M_{2n}) \, ds = 0 \end{aligned}}$$

Let us use (13) & (14) in (12) $\Rightarrow$

$$(15) \iiint_V \nabla \phi \cdot \nabla \phi \, dV = 0 \text{ Now using (7), (15) can be written as } (16)$$

$$\iiint_V -\vec{W} \cdot (-\vec{W}) \, dV = 0 \Rightarrow \iiint_V \vec{W} \cdot \vec{W} \, dV = 0 \Rightarrow \iiint_V |\vec{W}|^2 \, dV = 0$$

Since the norm of a vector $|\vec{W}|^2$ can not be negative,

the only way we can satisfy (16) is $\vec{W} = 0 \Rightarrow \vec{M}_1 = \vec{M}_2$

Problem #5)

$$\nabla^2 V = \frac{1}{R^2} \frac{\partial}{\partial R} R^2 \frac{\partial V}{\partial R} + \frac{1}{R^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{R^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$$

For $V = \frac{1}{|\vec{R}|} = \frac{1}{R}$ then $\frac{\partial}{\partial \theta} \rightarrow 0$ $\frac{\partial}{\partial \phi} \rightarrow 0 \Rightarrow$

$$\nabla^2 \frac{1}{R} = \frac{1}{R^2} \frac{\partial}{\partial R} R^2 \left(\frac{\partial}{\partial R} \frac{1}{R} \right) = \frac{1}{R^2} \frac{\partial}{\partial R} R^2 \left[-\frac{1}{R^2} \right] = \frac{1}{R^2} \frac{\partial}{\partial R} (-1) = 0$$

For $R \neq 0 \Rightarrow \boxed{\nabla^2 \frac{1}{R} = 0 \text{ for } R \neq 0}$

But for $R=0$, $\frac{1}{R}$ & hence $\nabla^2 \frac{1}{R}$ is singular.

Note the following:

$$\nabla^2 \left(\frac{1}{R} \right) = \nabla \cdot \left(\nabla \frac{1}{R} \right) \Rightarrow \iiint_V \nabla^2 \frac{1}{R} dV = \iiint_V \nabla \cdot \left(\nabla \frac{1}{R} \right) dV^3 \Rightarrow$$

$$\iiint_V \nabla^2 \frac{1}{R} dV^3 = \oint_S \nabla \frac{1}{R} \cdot \vec{ds} \quad \text{where } S \text{ is the surface bounding volume } V$$

using divergence theorem

* It also can be shown $\nabla \left(\frac{1}{R} \right) = -\frac{\hat{R}}{R^2}$ where $\hat{R}$ is the unit normal vector in direction $\vec{R}$

$$\iiint_V \nabla^2 \frac{1}{R} dV^3 = \oint_S \nabla \frac{1}{R} \cdot \vec{ds} = \oint_S -\frac{\hat{R}}{R^2} \cdot \vec{ds}$$

$$= \oint_S -\frac{\hat{R}}{R^2} \cdot R^2 \sin \theta d\theta d\phi \hat{R}$$

where $\vec{ds} = R^2 \sin \theta d\theta d\phi \hat{R}$
for integration over the surface of the sphere

$$\iiint \nabla^2 \frac{1}{R} dv^3 = \int_0^\pi \int_0^{2\pi} -\sin\theta d\theta d\phi$$

$$\theta=0, \phi=0$$

$$(2) \quad = -4\pi \quad \text{hence}$$

$$\boxed{\iiint \nabla^2 \frac{1}{R} dv^3 = -4\pi}$$

We now have shown that $\nabla^2 \frac{1}{R} = 0$ for all points -

with exception of $R=0$ & that its integral is -4π for the case of $R=0$. This is the property of Delta function for which $\delta(R)=0$ for $R \neq 0$ &

$$3) \quad \iiint_V \delta(R) dv^3 = 1 \quad \text{In other words we can write (2)}$$

$$\Rightarrow -\frac{1}{4\pi} \iiint \nabla^2 \frac{1}{R} dv^3 = 1 \quad \& \text{ Compare to (2)}$$

$$\iiint \delta^3(R) dv^3 = 1 \Rightarrow$$

$$-\frac{1}{4\pi} \nabla^2 \frac{1}{R} = \delta^3(R) \Rightarrow -\nabla^2 \frac{1}{R} = 4\pi \delta^3(R)$$

Problem 6)

(a) Start with continuity Eq

$$\textcircled{1} \nabla \cdot \vec{J} + \frac{\partial \rho_{ev}}{\partial t} = 0 \quad \text{where} \quad \textcircled{2} \vec{J} = \sigma \vec{E} \Rightarrow$$

$$\textcircled{3} \nabla \cdot \sigma \vec{E} + \frac{\partial \rho_{ev}}{\partial t} = 0 \Rightarrow \textcircled{4} \sigma \nabla \cdot \vec{E} + \frac{\partial \rho_{ev}}{\partial t} = 0 \quad \text{but} \quad \textcircled{5} \nabla \cdot \vec{E} = \rho_{ev} / \epsilon \Rightarrow$$

$$\textcircled{6} \boxed{\frac{\sigma}{\epsilon} \rho_{ev} + \frac{\partial \rho_{ev}}{\partial t} = 0}$$

(b) The solution for $\textcircled{7} \frac{\partial \rho_{ev}}{\partial t} = -\frac{\sigma}{\epsilon} \rho_{ev}$ is given by

$$\textcircled{8} \rho_{ev} = \rho_0 e^{-\frac{\sigma}{\epsilon} t} \quad \text{where } \rho_0 \triangleq \text{initial charge distribution is a constant}$$

we define $\textcircled{9} \tau = \epsilon / \sigma$ then

$$\textcircled{10} \boxed{\rho_{ev} = \rho_0 e^{-\frac{\sigma}{\epsilon} t} = \rho_0 e^{-t/\tau}}$$

(c) Eq. (10) states that if charge density ρ_0 is placed inside the metal, its distribution will decrease with time in an exponential manner, i.e. the charges move to the metal surface & redistribute themselves such that $\vec{E}$ inside of metal is zero. The time constant for this redistribution is proportional to $\tau = \frac{\epsilon}{\sigma}$, i.e. the more conductive a metal, the faster charge redistribution. For copper, charge density reaches e^{-1} (36.8% of original value) at $\tau = \frac{\epsilon}{\sigma} = \frac{\epsilon_0}{\sigma} = \frac{8.85 \times 10^{-12}}{5.8 \times 10^7} \approx 1.5 \times 10^{-19} \text{ [s]}$